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HYDRAULIC MOTOR FOR HEAVY DUTY APPLICATION

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OPERATING RECOMMENDATIONS

OIL TYPE

Hydraulic oils with anti-wear, anti-foam and demulsifiers are recommended for systems incorporating Impro Fluidtek motors. Straight oils can be used but may require VI (viscosity index) improvers depending on the operating temperature range of the system. Other water based and environmentally friendly oils may be used, but service life of the motor and other components in the system may be significantly shortened. Before using any type of fluid, consult the fluid requirements for all components in the system for compatibility. Testing under actual operating conditions is the only way to determine if acceptable service life will be achieved.

FLUID VISCOSITY & FILTRATION

Fluids with a viscosity between 20 - 43 cSt [100 - 200S.U.S.] at operating temperature is recommended. Fluid temperature should also be maintained below 85°C [180°F]. It is also suggested that the type of pump and its operating specifications be taken into account when choosing a fluid for the system. Fluids with high viscosity can cause cavitation at the inlet side of the pump. Systems that operate over a wide range of temperatures may require viscosity improvers to provide acceptable fluid performance. Impro Fluidtek recommends maintaining an oil cleanliness level of ISO 17-14 or better.

INSTALLATION & START-UP

When installing an Impro Fluidtek motor it is important that the mounting flange of the motor makes full contact with the mounting surface of the application. Mounting hardware of the appropriate grade and size must be used. Hubs, pulleys, sprockets and couplings must be properly aligned to avoid inducing excessive thrust or radial loads. Although the output device must fit the shaft snug, a hammer should never be used to install any type of output device onto the shaft. The port plugs should only be removed from the motor when the system connections are ready to be made. To avoid contamination, remove all matter from around the ports of the motor and the threads of the fittings. Once all system connections are made, it is recommended that the motor be run-in for 15-30 minutes at no load and half speed to remove air from the hydraulic system.

MOTOR PROTECTION

Over-pressurization of a motor is one of the primary causes of motor failure. To prevent these situations, it is necessary to provide adequate relief protection for a motor based on the pressure ratings for that particular model. For systems that may experience overrunning conditions, special precautions must be taken. In an overrunning condition, the motor functions as a pump and attempts to convert kinetic energy into hydraulic energy. Unless the system is properly configured for this condition, damage to the motor or system can occur. To protect against this condition a counterbalance valve or relief cartridge must be incorporated into the circuit to reduce the risk of over-pressurization. If a relief cartridge is used, it must be installed upline of the motor, if not in the motor, to relieve the pressure created by the over-running motor. To provide proper motor protection for an over-running load application, the pressure setting of the pressure relief valve must not exceed the intermittent rating of the motor.

HYDRAULIC MOTOR SAFETY PRECAUTION

A hydraulic motor must not be used to hold a suspended load. Due to the necessary internal tolerances, all hydraulic motors will experience some degree of creep when a load induced torque is applied to a motor at rest. All applications that require a load to be held must use some form of mechanical brake designed for that purpose.



MOTOR/BRAKE PRECAUTION

Caution! - Impro Fluidtek motor/brakes are intended to operate as static or parking brakes. System circuitry must be designed to bring the load to a stop before applying the brake.

Caution! - Because it is possible for some large displacement motors to overpower the brake, it is critical that the maximum system pressure be limited for these applications. Failure to do so could cause serious injury or death. When choosing a motor/brake for an application, consult the performance chart for the series and displacement chosen for the application to verify that the maximum operating pressure of the system will not allow the motor to produce more torque than the maximum rating of the brake. Also, it is vital that the system relief be set low enough to insure that the motor is not able to overpower the brake.

To ensure proper operation of the brake, a separate case drain back to tank must be used. Use of the internal drain option is not recommended due to the possibility of return line pressure spikes. A simple schematic of a system utilizing a motor/brake is shown on page 6. Although maximum brake release pressure may be used for an application, a 34 bar [500 psi] pressure reducing valve is recommended to promote maximum life for the brake release piston seals. However, if a pressure reducing valve is used in a system which has case drain back pressure, the pressure reducing valve should be set to 34 bar [500 psi] over the expected case pressure to ensure full brake release. To achieve proper brake release operation, it is necessary to bleed out any trapped air and fill brake release cavity andhoses before all connections are tightened. To facilitate this operation, all motor/brakes feature two release ports. One or both of these ports may be used to release the brake in the unit. Motor/brakes should be configured so that the release ports are near the top of the unit in the installed position.



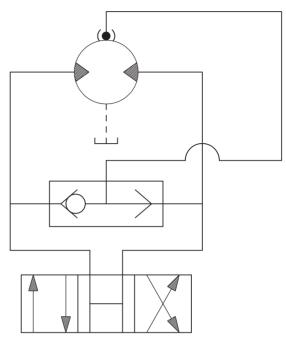
OPERATING RECOMMENDATIONS & MOTOR CONNECTIONS

Once all system connections are made, one release port must be opened to atmosphere and the brake release line carefully charged with fluid until all air is removed from the line and motor/brake release cavity. When this has been accomplished the port plug or secondary release line must be reinstalled. In the event of a pump or battery failure, an external pressure source may be connected to the brake release port to release the brake, allowing the machine to be moved.

 NOTE: It is vital that all operating recommendations be followed. Failure to do so could result in injury or death.

MOTOR CIRCUITS

There are two common types of circuits used for connecting multiple numbers of motors – series connection and parallel connection.

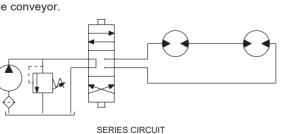


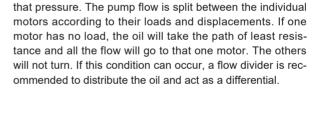
TYPICAL MOTOR/BRAKE SCHEMATIC

PARALLEL CONNECTION

SERIES CONNECTION

When motors are connected in series, the outlet of one motor is connected to the inlet of the next motor. This allows the full pump flow to go through each motor and provide maximum speed. Pressure and torque are distributed between the motors based on the load each motor is subjected to. The maximum system pressure must be no greater than the maximum inlet pressure of the first motor. The allowable back pressure rating for a motor must also be considered. In some series circuits the motors must have an external case drain connected. A series connection is desirable when it is important for all the motors to run the same speed such as on a long line conveyor.

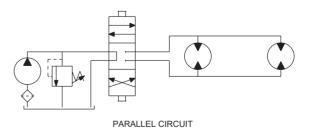




In a parallel connection all of the motor inlets are connected.

This makes the maximum system pressure available to

each motor allowing each motor to produce full torque at

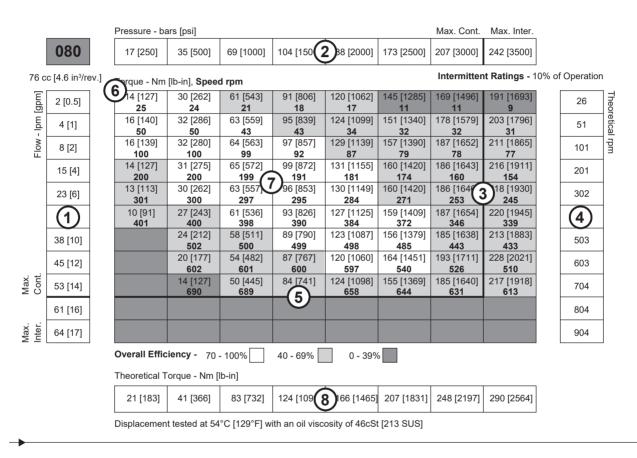


NOTE: The motor circuits shown above are for illustration purposes only. Components and circuitry for actual applications may vary greatly and should be chosen based on the application.



PRODUCT TESTING

Performance testing is the critical measure of a motor's ability to convert flow and pressure into speed and torque. All product testing is conducted using an Impro Fluidtek state of the art test facility. This facility utilizes fully automated test equipment and custom designed software to provide accurate, reliable test data. Test routines are standardized, including test stand calibration and stabilization of fluid temperature and viscosity, to provide consistent data. The example below provides an explanation of the values pertaining to each heading on the performance chart.



- 1. Flow represents the amount of fluid passing through the motor during each minute of the test.
- 2. Pressure refers to the measured pressure differential between the inlet and return ports of the motor during the test.
- 3. The maximum continuous pressure rating and maximum intermittent pressure rating of the motor are separated by the dark lines on the chart.
- 4. Theoretical RPM represents the RPM that the motor would produce if it were 100% volumetrically efficient. Measured RPM divided by the theoretical RPM give the actual volumetric efficiency of the motor.
- 5. The maximum continuous flow rating and maximum intermittent flow rating of the motor are separated by the dark line on the chart.
- 6. Performance numbers represent the actual torque and speed generated by the motor based on the corresponding input pressure and flow. The numbers on the top row indicate torque as measured in Nm [Ib-in], while the bottom number represents the speed of the output shaft.
- 7. Areas within the white shading represent maximum motor efficiencies.
- 8. Theoretical Torque represents the torque that the motor would produce if it were 100% mechanically efficient. Actual torque divided by the theoretical torque gives the actual mechanical efficiency of the motor.



ALLOWABLE BEARING & SHAFT LOADING

This catalog provides curves showing allowable radial loads at points along the longitudinal axis of the motor. They are dimensioned from the mounting flange. Two capacity curves for the shaft and bearings are shown. A vertical line through the centerline of the load drawn to intersect the x-axis intersects the curves at the load capacity of the shaft and of the bearing.

In the example below the maximum radial load bearing rating is between the internal roller bearings illustrated with a solid line. The allowable shaft rating is shown with a dotted line.

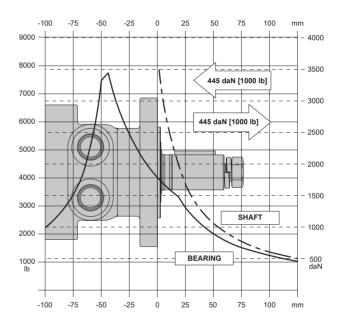
The bearing curves for each model are based on laboratory analysis and testing results constructed at Impro Fluidtek. The shaft loading is based on a 3:1 safety factor and 330 Kpsi tensile strength. The allowable load is the lower of the curves at a given point. For instance, one inch in front of the mounting flange the bearing capacity is lower than the shaft capacity. In this case, the bearing is the limiting load. The motor user needs to determine which series of motor to use based on their application knowledge.

ISO 281 RATINGS VS. MANUFACTURERS RATINGS

Published bearing curves can come from more than one type of analysis. The ISO 281 bearing rating is an international standard for the dynamic load rating of roller bearings. The rating is for a set load at a speed of 33 1/3 RPM for 500 hours (1 million revolutions). The standard was established to allow consistent comparisons of similar bearings between manufacturers. The ISO 281 bearing ratings are based solely on the physical characteristics of the bearings, removing any manufacturers specific safety factors or empirical data that influences the ratings.

Manufacturers' ratings are adjusted by diverse and systematic laboratory investigations, checked constantly with feedback from practical experience. Factors taken into account that affect bearing life are material, lubrication, cleanliness of the lubrication, speed, temperature, magnitude of the load and the bearing type.

The operating life of a bearing is the actual life achieved by the bearing and can be significantly different from the calculated life. Comparison with similar applications is the most accurate method for bearing life estimations.



EXAMPLE LOAD RATING FOR MECHANICALLY RETAINED NEEDLE ROLLER BEARINGS

Bearing Life $L_{10} = (C/P)^{p} [10^{6} revolutions]$

- L_{10} = nominal rating life
- C = dynamic load rating
- P = equivalent dynamic load
- Life Exponent ^p = 10/3 for needle bearings

BEARING LOAD MULTIPLICATION FACTOR TABLE										
RPM	FACTOR	RPM	FACTOR							
50	1.23	500	0.62							
100	1.00	600	0.58							
200	0.81	700	0.56							
300	0.72	800	0.50							
400	0.66									



VEHICLE DRIVE CALCULATIONS

When selecting a wheel drive motor for a mobile vehicle, a number of factors concerning the vehicle must be taken into consideration to determine the required maximum motor RPM, the maximum torque required and the maximum load each motor must support. The following sections contain the necessary equations to determine this criteria. An example is provided to illustrate the process.

Sample application (vehicle design criteria)

Vehicle description	4 wheel vehicle
GVW	1,500 lbs.
Rolling radius of tires	16 in.
Top speed	5 mph
Worst working surface	poor asphalt

2 wheel drive
425 lbs.
0-5 mph in 10 sec.

To determine maximum motor speed

$$RPM = \frac{2.65 \times KPH \times G}{rm}$$

MPH = Max. vehicle speed (miles/hr) G = Gear reduction ratio (if none, G = 1)

 $\frac{168 \times 5 \times 1}{52.5}$ RPM = Example 16

KPH = Max. vehicle speed (kilometers/hr) ri = Rolling radius of tire (inches) rm = Rolling radius of tire (meters)

To determine maximum torgue requirement of motor

168 x MPH x G

ri

To choose a motor(s) capable of producing enough torque to propel the vehicle, it is necessary to determine the Total Tractive Effort (TE) requirement for the vehicle.

To determine the total tractive effort, the following equation must be used:

TE = RR + GR + FA + DP (lbs or N)

Where:

Where:

TE = Total tractive effort GR = Force required to climb a grade

RR = Force necessary to overcome rolling resistance FA = Force required to accelerate

DP = Drawbar pull required

The components for this equation may be determined using the following steps:

Step One: Determine Rolling Resistance

Rolling Resistance (RR) is the force necessary to propel a vehicle over a particular surface. It is recommended that the worst possible surface type to be encountered by the vehicle be factored into the equation.

$$RR = \frac{GVW}{1000} \times R \text{ (lb or N)}$$

GVW = Gross (loaded) vehicle weight (lb or kg)

R = Surface friction (value from Rolling Resistance)

Example RR =
$$\frac{1500}{1000}$$
 X 22 lbs = 33 lbs

Rolling Resistance						
Concrete (excellent)10	Cobbles (ordinary)55					
Concrete (good)15	Cobbles (poor)37					
Concrete (poor)20	Snow (2 inch)25					
Asphalt (good)12	Snow (4 inch)37					
Asphalt (fair)17	Dirt (smooth)25					
Asphalt (poor)22	Dirt (sandy)37					
Macadam (good)15	Mud37 to 150					
Macadam (fair)22	Sand (soft)60 to 150					
Macadam (poor)37	Sand (dune)160 to 300					

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Step Two: Determine Grade Resistance

Grade Resistance (GR) is the amount of force necessary to move a vehicle up a hill or "grade." This calculation must be made using the maximum grade the vehicle will be expected to climb in normal operation.

To convert incline degrees to % Grade:

% Grade = [tan of angle (degrees)] x 100

 $GR = \frac{\% \text{ Grade}}{100} \times \text{ GVW (lb or N)}$ $\boxed{\text{Example} \quad RR = \frac{20}{100} \times 1500 \text{ lbs} = 300 \text{ lbs}}$

Step Three: Determine Acceleration Force

Acceleration Force (FA) is the force necessary to accelerate from a stop to maximum speed in a desired time.

 $FA = \frac{MPH \times GVW (Ib)}{22 \times t} \qquad FA = \frac{KPH \times GVW (N)}{35.32 \times t}$

Where:

t = Time to maximum speed (seconds)

Example FA = $\frac{5 \times 1500 \text{ lbs}}{22 \times 10}$ = 34 lbs

Step Four: Determine Drawbar Pull

Drawbar Pull (DP) is the additional force, if any, the vehicle will be required to generate if it is to be used to tow other equipment. If additional towing capacity is required for the equipment, repeat steps one through three for the towable equipment and sum the totals to determine DP.

Step Five: Determine Total Tractive Effort

The Tractive Effort (TE) is the sum of the forces calculated in steps one through three above. On low speed vehicles, wind resistance can typically be neglected. However, friction in drive components may warrant the addition of 10% to the total tractive effort to insure acceptable vehicle performance.

TE = RR + GR + FA + DP (lb or N)

Example TE = 33 + 300 + 34 + 0 (lbs) = 367 lbs

Step Six: Determine Motor Torque

The Motor Torque (T) required per motor is the Total Tractive Effort divided by the number of motors used on the machine. Gear reduction is also factored into account in this equation.

 $T = \frac{TE \times ri}{M \times G}$ Ib-in per motor $T = \frac{TE \times rm}{M \times G}$ Nm per motor

Where:

M = Number of driving motors

Example T = $\frac{367 \times 16}{2 \times 1}$ lb-in / motor = 2936 lb-in

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Step Seven: Determine Wheel Slip

To verify that the vehicle will perform as designed in regards to tractive effort and acceleration, it is necessary to calculate wheel slip (TS) for the vehicle. In special cases, wheel slip may actually be desirable to prevent hydraulic system overheating and component breakage should the vehicle become stalled.

 $TS = \frac{W x f x ri}{G}$

 $\frac{ri}{G} TS = \frac{W x f x rm}{G}$ (Nm per motor)

(lb-in per motor)

Where:

f = Coefficient of friction

W = Loaded vehicle weight over driven wheel (lb or N)

Example TS = $\frac{425 \times .06 \times 16}{1}$ lb-in / motor = 4080 lbs

Coefficient of friction (f)
Steel on steel
Rubber tire on dirt 0.5
Rubber tire on dirt 0.5 Rubber tire on a hard surface. 0.6 - 0.8 Rubber tire on cement 0.7
Rubber tire on cement0.7

To determine radial load capacity requirement of motor

When a motor used to drive a vehicle has the wheel or hub attached directly to the motor shaft, it is critical that the radial load capabilities of the motor are sufficient to support the vehicle. After calculating the Total Radial Load (RL) acting on the motors, the result must be compared to the bearing/shaft load charts for the chosen motor to determine if the motor will provide acceptable load capacity and life.

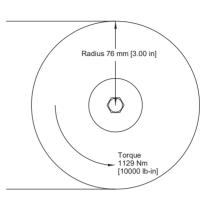
$RL = \sqrt{W^2}$	$+ \left(\frac{T}{ri}\right)^2$ lb	$RL = \sqrt{W^2 + }$	$\left(\frac{T}{rm}\right)^2$	kg
Example	$RL = \sqrt{425^2}$	$+\left(\frac{2936}{16}\right)^2 = 463$	lbs	

Once the maximum motor RPM, maximum torque requirement, and the maximum load each motor must support have been determined, these figures may then be compared to the motor performance charts and to the bearing load curves to choose a series and displacement to fulfill the motor requirements for the application.

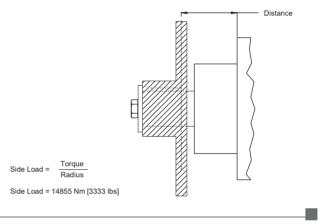


INDUCED SIDE LOAD

In many cases, pulleys or sprockets may be used to transmit the torque produced by the motor. Use of these components will create a torque induced side load on the motor shaft and bearings. It is important that this load be taken into consideration when choosing a motor with sufficient bearing and shaft capacity for the application.



To determine the side load, the motor torque and pulleyor sprocket radius must be known. Side load may be calculated using the formula below. The distance from the pulley/sprocket centerline to the mounting flange of the motor must also be determined. These two figures may then be compared to the bearing and shaft load curve of the desired motor to determine if the side load falls within acceptable load ranges.



HYDRAULIC EQUATIONS

Multiplication Factor	Abbrev.	Prefix
10 ¹²	Т	tera
10 ⁹	G	giga
10 ⁶	М	mega
10 ³	К	kilo
10 ²	h	hecto
10 ¹	da	deka
10 ⁻¹	d	deci
10-2	с	centi
10-3	m	milli
10-6	u	micro
10-9	n	nano
10 ⁻¹²	р	pico
10 ⁻¹⁵	f	femto
10-18	а	atto

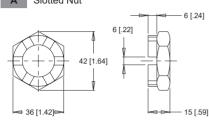
Theo. Speed (RPM) =-	1000 x LPM Displacement (cm³/rev)	or 231 x GPM Displacement (in³/rev)
Theo. Torque (lb-in) = ·	Bar x Disp. (cm³/rev) 20 pi	PSI x Displacement (in³/rev) 6.28
Power In (HP) =	Bar x LPM 600	or
Power Out (HP) =	Torque (Nm) x RPM 9543	or



SHAFT NUT INFORMATION

35MM TAPERED SHAFTS

M24 x 1.5 Thread A Slotted Nut



Torque Specifications: 32.5 daNm [240 ft.lb.]

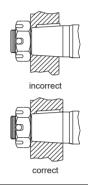
1" TAPERED SHAFTS

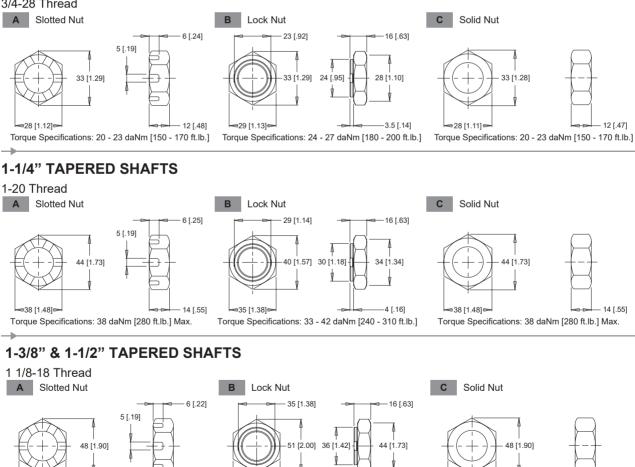
3/4-28 Thread

-

PRECAUTION

The tightening torques listed with each nut should only be used as a guideline. Hubs may require higher or lower tightening torque depending on the material. Consult the hub manufacturer to obtain recommended tightening torque. To maximize torque transfer from the shaft to the hub, and to minimize the potential for shaft breakage, a hub with sufficient thickness must fully engage the taper length of the shaft.





Torque Specifications: 34 - 48 daNm [250 - 350 ft.lb.]

4 [.16]

42 [1.66]∉

Torque Specifications: 41 - 54 daNm [300 - 400 ft.lb.]

Torque Specifications: 41 - 54 daNm [300 - 400 ft.lb.]

15 [.61]

44 [1.73]€

42 [1.66]∉

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15 [.61]

WT (All Series) Heavy Duty Hydraulic Motor



One of the most impressive features of the WT series is its remarkable torque potential despite its compact size. The WT series motor can generate a torque output comparable to that of competing designs, but in a smaller and lighter package. This space and weight efficiency does not compromise durability, as the motor utilizes substantial shafts, bearings, and links to efficiently transmit the powerful torque it produces. Additionally, the use of a drain reduces pressure on the shaft seal while ensuring optimal motor life through proper driveline lubrication. Furthermore, the WT series offers standard mounting and shaft options that are interchangeable with competing designs, and an internal drain option is also available.

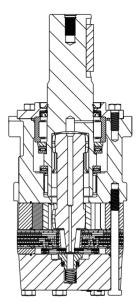
FEATURES / BENEFITS

- Heavy-duty roller bearings for extra side load capacity.
- · Best in class power to weight ratio due to compact design.
- · A variety of mounts and shafts provide flexibility in application design.
- Heavy-Duty Drive Link receives full flow lubrication to provide long service life.
- Optimized rotor geometry provides highly efficient smooth running performance.
- Three-zone Commutator Valve results in exceptional volumetric efficiency.
- Standard case and internal drain for extended shaft seal life.



SERIES DESCRIPTIONS

700 - Hydraulic Motor Standard



TYPICAL APPLICATIONS

Heavy-duty wheel drives, grain augers, sweepers, construction equipment, feed rollers, mixers, pumping units, conveyors, boring machines, rotators, mining equipment, forestry equipment and more.

CODE	Displacement cm ³ [in ³ /rev]						orque lb-in]		Max. Press bar [psi]	
	cui [inviev]	cont.	inter.	cont.	inter.	cont.	inter.	cont.	inter.	peak
300	300 [18.3]	320	380	95 [25]	114 [30]	819 [7250]	955 [8450]	207 [3000]	241 [3500]	259 [3750]
375	374 [22.8]	250	300	95 [25]	114 [30]	1045 [9250]	1127 [9975]	207 [3000]	224 [3250]	241 [3500]
470	464 [28.3]	464 [28.3] 200 240 95 [25] 114		114 [30]	1071 [9475]	1390 [12300]	172 [2500]	224 [3250]	241 [3500]	
540	536 [32.7]	180	210	95 [25]	114 [30]	1277 [11300]	1525 [13500]	172 [2500]	207 [3000]	241 [3500]
750	747 [45.6]	130	155	95 [25]	114 [30]	1835 [16240]	2138 [18923]	172 [2500]	207 [3000]	241 [3500]
930	929 [56.7]	100	120	95 [25]	114 [30]	1780 [15750]	2141 [18950]	138 [2000]	172 [2500]	207 [3000]
1K1	1047 [63.9]	93	112	95 [25]	114 [30]	2041 [18064]	2308 [20428]	138 [2000]	172 [2500]	207 [3000]
1K5	1495 [91.2]	60	70	95 [25]	114 [30]	2090 [18500]	2316 [20500]	103 [1500]	121 [1750]	138 [2000]
2K1	2093 [127.7]	40	50	95 [25]	114 [30]	2661 [23550]	3342 [29580]	103 [1500]	121 [1750]	138 [2000]

SPECIFICATIONS

Performance data is typical. Performance of production units varies slightly from one motor to another. See page 7 for additional information on product testing. Running at intermittent ratings should not exceed 10% of every minute of operation.





DISPLACEMENT PERFORMANCE

			Pressure - ba	ars [psi]					Max. Cont.	Max. Inter.			
	300		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	241 [3500]			
300 cm ³	³ [18.3 in ³ /re	ev.]	Torque - Nm	[lb-in], Spee	d rpm				Intermitter	nt Ratings - 1	0% of C	Operatio	n
[mdß	2 [0.5]		54 [476] 4	115 [1014] 3	237 [2100] 2							7	Theo
Flow - lpm [gpm]	4 [1]		47 [415] 11	108 [952] 9	255 [2256] 7	380 [3363] 5	486 [4304] 3					13	Theoretical rpm
Flow	8 [2]		49 [435] 24	119 [1057] 23	257 [2278] 21	410 [3628] 19	543 [4801] 15	671 [5942] 12	789 [6983] 9	899 [7959] 7		26	rpm
	15 [4]		49 [430] 50	120 [1064] 49	264 [2336] 46	409 [3616] 43	554 [4904] 37	701 [6202] 32	839 [7424] 28	971 [8595] 26		51]
	23 [6]			116 [1025] 75	278 [2462] 69	420 [3719] 65	567 [5019] 58	712 [6297] 54	854 [7554] 51	983 [8701] 48		76	
	30 [8]			105 [929] 100	251 [2222] 97	396 [3506] 93	542 [4793] 86	692 [6122] 78	831 [7353] 70	974 [8621] 69		101	
	38 [10]			99 [877] 126	237 [2099] 122	388 [3438] 115	549 [4857] 113	687 [6081] 107	833 [7369] 96	970 [8588] 90		127	
	45 [12]			88 [762] 151	237 [2094] 150	378 [3342] 140	527 [4666] 135	666 [5893] 129	823 [7281] 119	963 [8523] 113		152	
	53 [14]			77 [679] 176	211 [1864] 175	361 [3191] 172	506 [4478] 164	656 [5802] 156	805 [7121] 151	951 [8420] 140		177	
	61 [16]			60 [528] 201	208 [1845] 200	359 [3179] 189	495 [4378] 185	648 [5731] 178	791 [6999] 172	928 [8213] 165		202	
	68 [18]				191 [1694] 225	335 [2961] 222	497 [4402] 211	632 [5592] 156	776 [6871] 196	914 [8093] 189		228	
	76 [20]				168 [1489] 251	320 [2835] 247	461 [4083] 240	610 [5401] 233	764 [6762] 228	897 [7934] 216		253	
	83 [22]				147 [1298] 276	302 [2675] 272	444 [3926] 269	588 [5205] 258	742 [6570] 249	883 [7810] 234		278	
	91 [24]				123 [1086] 300	272 [2409] 298	414 [3666] 296	558 [4934] 290	708 [6264] 281	851 [7535] 272		303	
Max. Cont.	95 [25]				108 [958] 315	257 [2278] 313	393 [3482] 308	549 [4857] 300	694 [6139] 289	839 [7421] 280		316	
Max. Inter.	114 [30]					186 [1642] 376	333 [2945] 372	473 [4189] 369				379	
			Overall Effic	iency - 70	- 100%	40 - 69%	0 - 39%	6					
	Rotor Width		Theoretical T	orque - Nm [lb-in]								
	25.4 [1.000]		82 [729]	165 [1457]	329 [2914]	494 [4371]	659 [5828]	823 [7285]	988 [8742]	1152 [10199]			
	mm [in]		Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cS	t [213 SUS]					

WT (All Series)



Heavy Duty Hydraulic Motor

DISPLACEMENT PERFORMANCE

			Pressure - ba	ars [psi]					Max. Cont.	Max. Inter.			
	375		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	224 [3250]			
375 cm ³	375 cm ³ [22.8 in ³ /rev.] Torque - Nm [lb-in], Speed rpm								Intermitter	nt Ratings - 1	0% of (Operatior	n
[mdß	2 [0.5]		65 [574] 4	144 [1272] 3	302 [2670] 2	449 [3970] 1					Γ	6	Theo
Flow - Ipm [gpm]	4 [1]		66 [583] 9	152 [1345] 8	312 [2757] 7	475 [4208] 5	625 [5535] 4				Γ	11	Theoretical
Flow .	8 [2]		67 [596] 19	154 [1365] 18	329 [2907] 17	496 [4388] 14	644 [5695] 12	805 [7122] 10	963 [8524] 8	1050[9288] 7		21	rpm
	15 [4]		71 [627] 40	158 [1400] 39	337 [2982] 37	513 [4536] 34	680 [6020] 30	858 [7596] 27	1013 [8962] 25	1099[9723] 23		41	1
	23 [6]		64 [570] 60	151 [1334] 60	336 [2969] 58	520 [4598] 54	694 [6141] 49	871 [7704] 45	1048 [9275] 41	1115[9867] 41		61]
	30 [8]		53 [467] 81	151 [1337] 80	325 [2876] 78	512 [4532] 73	691 [6113] 69	873 [7724] 63	1051 [9304] 60	1126[9964] 59		82]
	38 [10]			131 [1161] 101	313 [2768] 99	502 [4439] 95	686 [6075] 89	884 [7824] 82	1049 [9281] 79	1131[10011] 77		102]
	45 [12]			112 [995] 121	308 [2725] 120	494 [4375] 116	685 [6059] 109	862 [7626] 103	1053 [9321] 98	1137[10066] 97		122]
	53 [14]			99 [878] 141	283 [2508] 140	469 [4149] 136	645 [5705] 131	844 [7467] 125	1013 [8965] 117	1116[9877] 115		142]
	61 [16]			75 [662] 162	262 [2319] 161	443 [3923] 160	631 [5587] 155	823 [7283] 148	1009 [8930] 143	1114[9859] 136		163]
	68 [18]				248 [2198] 181	427 [3779] 178	612 [5416] 175	804 [7119] 167	1005 [8895] 160	1091[9653] 156		183]
	76 [20]				218 [1925] 202	403 [3568] 200	583 [5161] 195	778 [6886] 189	966 [8549] 178	1071[9474] 173		203]
	83 [22]				189 [1676] 222	375 [3318] 221	561 [4967] 217	754 [6669] 211	942 [8335] 201	1036[9171] 96		223	
	91 [24]				155 [1374] 242	344 [3041] 240	535 [4732] 237	724 [6410] 229				244	
Max. Cont.	95 [25]					321 [2839] 252	519 [4596] 249	710 [6283] 241				254	
Max. Inter.	114 [30]					238 [2110] 303	432 [3820] 301	622 [5503] 296				304	
				ioney 70	4000/	4000%	-	,					
	Rotor		Overall Effic Theoretical T			40 - 69%	0 - 39%	0					
	Width 31.8				-								
	[1.252]		103 [908]	205 [1815]	410 [3631]	615 [5446]	821 [7261]	1026 [9076]	1231 [10892]	1333 [11799]			
	mm [in]		Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cS	t [213 SUS]					



DISPLACEMENT PERFORMANCE

			Pressure - ba	ars [psi]					Max. Cont.	Max. Inter.			
	470		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]	224 [3250]			
465 cm ³	³ [28.3 in ³ /re	ev.]	Torque - Nm	[lb-in], Speed	d rpm				Intermitter	nt Ratings - 1	0% of	Operatior	n
[mdß]	2 [0.5]		86 [762] 3	201 [1780] 2	401 [3553] 2						[5	Theo
Flow - Ipm [gpm]	4 [1]		92 [817] 7	195 [1728] 7	406 [3597] 6	610 [5395] 5	806 [7137] 4					9	Theoretical rpm
Flow	8 [2]		94 [835] 15	199 [1761] 15	14	631 [5580] 13	832 [7365] 11	1042 [9226] 9	1239 [10961] 8			17	lub
	15 [4]		92 [815] 32	202 [1784] 32	426 [3769] 60	646 [5717] 28	849 [7513] 24	1066 [9430] 23	1272 [11256] 21	1381 [12217] 19		33	
	23 [6]		82 [729] 48	203 [1799] 47	423 [3744] 46	647 [5725] 43	855 [7565] 39	1070 [9473] 36	1275 [11287] 34	1365 [12083] 32		49]
	30 [8]		67 [595] 65	185 [1641] 64	414 [3663] 63	642 [5683] 60	867 [7671] 54	1078 [9538] 47	1300 [11508] 46	1398 [12367] 44		66	1
	38 [10]		52 [459] 81	170 [1503] 80	399 [3532] 79	630 [5573] 78	857 [7584] 69	1077 [9531] 63	1283 [11352] 61	1393 [12323] 58		82]
	45 [12]			153 [1354] 97	380 [3366] 96	613 [5422] 93	842 [7454] 88	1072 [9488] 77	1302 [11523] 74	1394 [12334] 68		98]
	53 [14]			127 [1121] 114	359 [3173] 113	591 [5229] 110	823 [7282] 104	1057 [9350] 97	1270 [11242] 89	1392 [12318] 85		114]
	61 [16]			100 [888] 160	335 [2964] 129	564 [4993] 127	798 [7061] 119	1030 [9118] 114	1254 [11101] 108	1369 [12118] 102		131	1
	68 [18]			67 [595] 146	304 [2689] 145	535 [4734] 143	765 [6772] 137	1003 [8875] 132	1229 [10877] 120	1348 [11926] 114		147	1
	76 [20]				274 [2428] 162	504 [4458] 160	733 [6485] 155		1197 [10592] 139	1318 [11668] 136		164	1
	83 [22]				226 [2003] 178	458 [4050] 175	691 [6118] 172	928 [8215] 165	1150 [10181] 156	1266 [11200] 154		180	1
	91 [24]				176 [1554] 194	415 [3670] 192	669 [5917] 190	885 [7833] 183				196	1
Max. Cont.	95 [25]					389 [3442] 203	632 [5589] 198	867 [7676] 190				205	1
Max. Inter.	114 [30]					277 [2451] 243	514 [4549] 240	755 [6684] 235				245	1
2 - 1							_		1		L		
	Rotor		Overall Effic			40 - 69%	0 - 39%	6					
1	Width		Theoretical T	orque - Nm [l	b-in]								
	39.4 [1.553]		127 [1127]	255 [2253]	509 [4506]	764 [6760]	1018 [9013]	1273 [1126]	1528 [13519]	1655 [14646]			
	mm [in]		Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cS	t [213 SUS]					

WT (All Series)



Heavy Duty Hydraulic Motor

DISPLACEMENT PERFORMANCE

Pressure - bars [psi]						Max. Cont. Max. Inter.															
	540		17 [250]	35 [500]	69 [1000]	104 [1500]	138 [2000]	173 [2500]	207 [3000]												
536 cm ³ [32.7 in ³ /rev.] Torque - Nm [lb-in], Speed rpm Intermittent Ratings - 10% of Operation									n												
[mdß	2 [0.5]		103 [908] 2	215 [1607] 2	421 [3722] 1						4	Theo									
] mql .	4 [1]		104 [917] 6	228 [2016] 5	454 [4015] 4	666 [5897] 3	874 [7730] 1				8	Theoretical rpm									
Flow - lpm [gpm]	8 [2]		108 [954] 13	231 [2043] 12	474 [4191] 11	704 [6231] 9	925 [8190] 5	1153 [10201] 4			15	rpm									
	15 [4]		102 [906] 27	232 [2052] 26	503 [4448] 24	756 [6692] 21	994 [8799] 18	1221 [10806] 15	1461 [12930] 13		29										
	23 [6]		98 [866] 42	230 [2038] 41	498 [4404] 39		1023 [9049] 30		1494 [13219] 24	_	43	1									
	30 [8]		84 [744] 56	213 [1883] 55	484 [4280] 53			1273 [11262] 38			57										
	38 [10]		63 [561] 70	195 [1727] 69	466 [4122] 68		1006 [8903] 57	1285 [11374] 49	1532 [13556] 46		71	1									
	45 [12]		42 [373] 84	179 [1586] 83	444 [3928] 82	717 [6349] 76		1274 [11277] 65	1518 [13436] 57		85	1									
	53 [14]			146 [1295] 97	421 [3722] 95	694 [6139] 93		1253 [11091] 80			99	1									
	61 [16]			116 [1025] 113	391 [3460] 111	663 [5865] 108	930 [8230] 103	1206 [10675] 97			114	1									
	68 [18]			90 [798] 127	356 [3153] 125	629 [5563] 123	900 [7969] 116	-	1451 [12841] 100	-	128	1									
	76 [20]												56 [498] 141	330 [2923] 139	595 [5265] 137	-	1158 [10250] 123			142	1
	83 [22]				278 [2464] 155	549 [4859] 153	822 [7271] 148	1121 [9919] 136	1388 [12283] 133		156	1									
	91 [24]				243 [2154] 169	508 [4494] 166	794 [7024] 164	1054 [9325] 156			170	1									
Max. Cont.	95 [25]				220 [1948] 176	486 [4299] 174	762 [6741] 169	1025[9075] 163			177	1									
Max. Inter.	114 [30]				90 [800] 211	366 [3237] 210	638 [5649] 207	920 [8144] 203			212	1									
			Overall Effic	iency - 70		40 - 69%	0 - 39%	6		L		_									
	Rotor Width			orque - Nm [l																	
	45.5 [1.791]		147 [1302]	294 [2604]	588 [5207]	883 [7811]	1177[10414]	1471 [13018]	1765 [15621]												
	mm [in]	I	Displacemen	t tested at 54	°C [129°F] wi	ith an oil visc	osity of 46cS	t [213 SUS]													



DISPLACEMENT PERFORMANCE

er.
0]
- 10% of Operation
3 Theo
3 Theoretical ppm
11 Pm
21
95] 31
24] 41
55] 51
61
48] 71
82
45] 92
99] 102
87] 112
70] 122
45] 127
56] 152
83]

WT (All Series)



Heavy Duty Hydraulic Motor

DISPLACEMENT PERFORMANCE

		Pressure - ba	ars [psi]						Max. Cont.		Max. Inter.		
	930	17 [250]	35 [500]	52 [750]	69 [1000]	86 [1250]	104 [1500]	121 [1750]	138 [2000]	155 [2250]	173 [2500]		
929cm ³	[56.7 in ³ /rev.]	Torque - Nm	[lb-in], Speed	d rpm					Ir	ntermittent R	atings - 10%	of Operatior	n
gpm]	2 [0.5]	180 [1590] 1	387 [3423] 1	607 [5368] 1	801 [7089] 1							3	Theo
Flow - lpm [gpm]	4 [1]	196 [1734] 4	418 [3696]	653 [5780] 3	864 [7649] 3	1067 [9447] 3	1294 [11451] 3					5	Theoretical rpm
- wol	8 [2]	205 [1816] 8	442 [3907] 7	680 [6015] 7		1117 [9886]	1300 [11501] 6	1510 [13365] 5				9	l rpm
LL.	15 [4]	198 [1753]	432 [3825]	664 [5878]			1338 [11840]	1556 [13769]				17	1
	23 [6]	16 185 [1633]	16 420 [3719]	15 651 [5765]	908 [8034]				11 1794 [15873]			25	1
	30 [8]	24 162 [1438]	24 404 [3576]	24 636 [5624]		23 1107 [9800]						33	-
	38 [10]	32 125 [1109]	31 368 [3253]	30 626 [5536]	30 845 [7476]	29 1087 [9620]	28 1314 [11625]	27 1497 [13251]	24 1736 [15364]	22 1956 [17306]	17 2153 [19054]	41	-
	45 [12]	40 91 [807]	40 341 [3018]	39 578 [5111]	38 815 [7213]	38 1072 [9487]	36 1314 [11630]	34 1525 [13492]	31 1713 [15159]	28 1946 [17222]	24 2133 [18873]	49	-
		48 35 [310]	47 290 [2565]	46 533 [4715]	45 765 [6772]	44 1024 [9059]	42 1240 [10974]	41 1487 [13155]	36 1727 [15287]	33 1945 [17216]	32 2168 [19188]		-
	53 [14]	57	56 239 [2118]	55 484 [4281]	54	52	50	49	45 1696 [15008]	43	36	58	-
	61 [16]		64	63	62	61	59	57	54	50	46	66	
	68 [18]		205 [1811] 72	440 [3891] 72	701 [6202] 70	69	67	65	1643 [14538] 64	58	55	74	
	76 [20]		150 [1325] 81	409 [3616] 80	632 [5590] 79	801 [7091] 78	1100[9733] 76	1505 [12135] 75	1599 [14148] 72	1859 [16454] 67	2060 [18230] 63	82]
	83 [22]		99 [875] 89	336 [2977] 88					1561 [13816] 80			90	1
	91 [24]			282 [2497] 97	-			1266 [11201] 92	1489 [13179] 89			98	1
Max. Cont.	95 [25]			241 [2137] 101		722 [6390] 100			1454 [12863] 93			102	1
Max. N Inter. C	114 [30]			66 [582] 122	300 [2652] 121	532 [4711]				09	04	123	-
2 =				122	121	120	110	110					
		Overall Effic	iency - 70	- 100%	40 - 69%	0 - 39%	5						
	Rotor Width	Theoretical T	orque - Nm [l	lb-in]									
	78.9 [3.106]	255 [2257]	510 [4514]	765 [6771]	1020 [9029]	1275 [11286]	1530 [13543]	1785 [15800]	2040 [18057]	2296 [20314]	2551 [22572]		
	mm [in]	Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cSt	[213 SUS]						



DISPLACEMENT PERFORMANCE

		Pressure - ba	ars [psi]						Max. Cont.		Max. Inter.		
	1K1	17 [250]	35 [500]	52 [750]	69 [1000]	86 [1250]	104 [1500]	121 [1750]	138 [2000]	155 [2250]	173 [2500]		
1047cm	³ [63.9 in ³ /rev.]] Torque - Nm	[lb-in], Speed	d rpm					Ir	ntermittent R	atings - 10%	of Operatior	ı
[mdb	2 [0.5]	231 [2047] 2										2	Thec
Flow - lpm [gpm]	4 [1]	236 [2091]	489 [4328] 4	735 [6507] 3	961 [8506] 3							4	Theoretical
- wol	8 [2]	239 [2114] 8	509 [4502]		-	1249 [11053]	1492 [13202]					8	l rpm
ш.	15 [4]	233 [2062]		770 [6819]	1022 [8946]	1272 [11258]			1994 [17647]			15	-
	23 [6]	14 224 [1979]	14 493 [4363]			13 1285 [11377]						22	-
-	30 [8]	22 213 [1886]				21 1264 [11188]						29	-
-	38 [10]	29 207 [1831]	28 483 [4278]	29 746 [6598]	29 1004 [8356]	28 1264 [11186]	27 1529 [13534]	25 1774 [15699]	21 2027 [17940]	15 2309 [20432]	12 2528 [22373]	37	-
-		37 186 [1646]	37 461 [4082]	36 720 [6371]	36 973 [7915]	35 1249 [11055]	34 1511 [13377]	32 1761 [15582]	28 2022 [17896]	22 2247 [19887]	18 2500 [22129]		-
	45 [12]	44	44	44	43	43	42	41	38	33	27	44	
	53 [14]	161 [1424] 52	435 [3846] 52	694 [6140] 51	951 [7535] 51	1223[10821] 50	1490 [13188] 49	1746 [15450] 45	1988 [17597] 41	2219 [19641] 35	2462 [21793] 30	51	1
-	61 [16]	139 [1831] 60	410 [3624] 59	671 [5940] 59		1193[10558] 58						58	1
-	68 [18]		392 [3469] 66	654 [5790] 66		1172[10373] 65						66	1
	76 [20]		366 [3239] 74	624 [5518] 74		1141 [10095] 73						73	1
-	83 [22]		333 [2945]	587 [5197]	852 [5034]	1125 [9960]	1396[12352]	1642 [14535]	1894 [16767]	2120 [18762]	2389 [21263]	80	-
-	91 [24]		81 301 [2665]	81 551 [4878]		80 1076[9527]						87	-
Max. Cont.	95 [25]		89 270 [2392]	89 528 [4671]		87 1060[9382]						91	-
Max. M Inter. C	114 [30]		93 180 [1597]	92 437 [3867]	92 695 [1789]	92 967 [8557]		88 1485[13144]	83 1749 [15477]	77 2979 [17516]	69 2231 [19744]	109	-
LT X	114[00]		112	111	111	110	109	106	101	94	86	100	
		Overall Effic	iency - 70 -	- 100%	40 - 69%	0 - 39%	b						
	Rotor Width	Theoretical T	orque - Nm [l	b-in]	_								
	88.9 [3.502]	287 [2544]	575 [5088]	862 [7631]	1150 [10175]	1437 [12719]	1725 [15263]	2012 [17807]	2300 [20350]	2587 [22894]	2874 [25438]		
-	mm [in]	Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cSt	[213 SUS]						

WT (All Series)



Heavy Duty Hydraulic Motor

DISPLACEMENT PERFORMANCE

		Pressure - b	ars [psi]				Max. Cont.	Max. Inter.		
	1K5	17 [250]	35 [500]	52 [750]	69 [1000]	86 [1250]	104 [1500]	121 [1750]		
1495cm	³ [91.2in ³ /rev.	Torque - Nm	[lb-in], Spee	d rpm			Intermitten	t Ratings - 10	ე% of Opera	tion
[gpm]	2 [0.5]	305 [2703] 0.9	648 [5736] 0.6						2	Theo
Flow - lpm [gpm]	4 [1]	336 [2978] 2	693 [6128] 1	1011 [8942] 1					3	Theoretical rpm
Flow	8 [2]	351 [3106] 4	729 [6454] 4	1085 [9597] 3	1364 [12072] 3				6	rpm
	15 [4]	331 [2925] 9	712 [6304] 9	1116 [9879] 8	1491 [13191] 7	1771 [15668] 7			11	
	23 [6]	297 [2629] 15	681 [3023] 14	1088 [9632] 13	1464 [12952] 12	1770 [15662] 10			16	
	30 [8]	247 [2183] 20	640 [5662] 19	1038 [9188] 18	1430 [12655] 17	1793 [15864] 15	2123 [18786] 9		21	
	38 [10]	197 [1740] 25	583 [5159] 24	1001 [8860] 23	1377 [12189] 22	1749 [15479] 19	2090 [18498] 14		26	
	45 [12]	131 [1157] 30	531 [4695] 29	940 [8315] 28	1330 [11770] 27	1702 [15066] 24	2041 [18059] 19	2329 [20613] 14	31	
	53 [14]	67 [594] 36	484 [4282] 35	869 [7689] 33	1267 [11217] 32	1642 [14532] 30	1990 [17612] 24	2300 [20353] 15	36	
	61 [16]		391 [3457] 40	769 [6805] 39	1172 [10374] 37	1567 [13866] 36	1914 [16941] 32	2258 [19986] 21	41	
	68 [18]		294 [2602] 45	686 [6072] 44	1076 [9523] 43	1489 [13177] 40	1846 [16334] 38	2188 [19366] 27	46	
	76 [20]		182 [1607] 50	614 [5435] 49	988 [8746] 48	1392 [12320] 47	1743 [15429] 44	2301 [18553] 37	51	
	83 [22]		87 [770] 55	487 [4310] 54	872 [7720] 53	1283 [11356] 52	1632 [14442] 48	2021 [17883] 46	56	
	91 [24]			456 [4032] 60	749[6632] 60	1146 [10143] 58	1533 [13570] 58	1872 [16568] 50	61	
Max. Cont.	95 [25]			293 [2589] 63	704 [6232] 62	1052[9313] 62	1465 [12961] 59	1843 [16306] 53	64	
Max. Inter.	114 [30]				246[2174] 75	645[5711] 74	1047 [9265] 73		76	
	Rotor	Overall Effic	ciency - 70	- 100%	40 - 69%	0 - 39%	6			
	Width	Theoretical	Forque - Nm [lb-in]			1			
	127.1 [5.003]	410 [3631]	821 [7261]	1231 [10892]	1641 [14522]	2051 [18153]	2462 [21783]	2872 [25414]		
	mm [in]	Displacemer	nt tested at 54	°C [129°F] w	ith an oil visc	osity of 46cSt	t [213 SUS]			



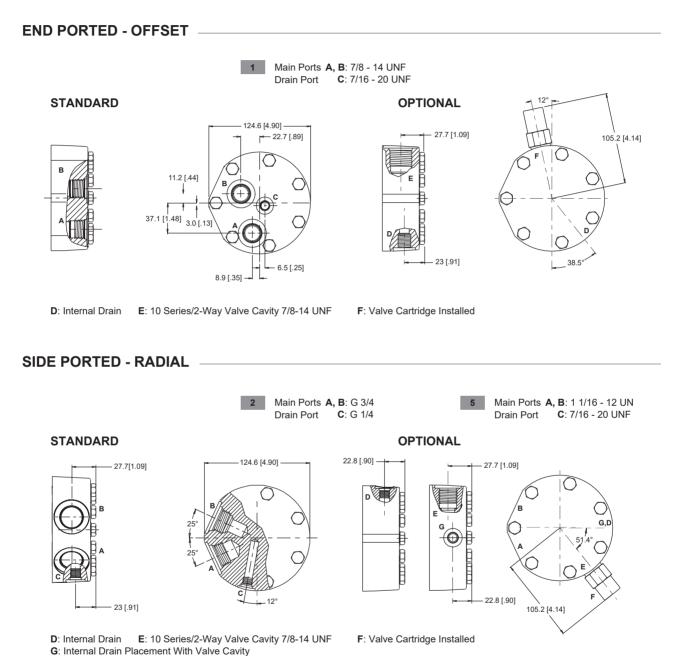
DISPLACEMENT PERFORMANCE

			Pressure - ba	ars [psi]				Max. Cont.	Max. Inter.			
	2K1		17 [250]	35 [500]	52 [750]	69 [1000]	86 [1250]	104 [1500]	121 [1750]			
2094cm	³ [127.7in ³	/rev.]	Torque - Nm	[lb-in], Speed	d rpm			Intermitten	it Ratings - 1	0% of Ope	eration	ı
	2 [0.5]]	438 [3878] 0.8	892 [7894] 0.8							1	The
Flow - Ipm [gpm]	4 [1]	-	440 [3891] 1		1398 [12375] 1						2	Theoretical rpm
- wol-	8 [2]		460 [4073] 3		1460 [12923] 3						4	l rpm
ш	15 [4]		443 [3920] 7		1491 [13192] 6	1980 [17520] 6					8	1
	23 [6]		402 [3560] 10	-	1470 [13012] 10	-					11	1
	30 [8]		337 [2985] 14			1920 [16995] 13	2390[21152] 9	2668 [23613] 8			15	1
	38 [10]		275 [2431] 17				2343[20733] 13				19	1
	45 [12]		173 [1535] 21				2286[20232] 17	2665 [23588] 12			22	1
	53 [14]		66 [587] 25				2206[19519] 21	2637 [23333] 13			26	1
	61 [16]				1018[9009] 28	-	2107[18645] 26	2574 [22777] 20			29	
	68 [18]			368 [3257] 32	910[8052] 32		1980[17527] 30	-			33	1
	76 [20]			225 [1991] 36	755[6686] 36	1304 [11537] 36	1859[16449] 35				37	1
	83 [22]			71 [628] 39	622[5507] 39		1682[14885] 38	2212 [19575] 36			40	1
	91 [24]				429[3794] 43	984 [8704] 43	1544[13665] 42	2067 [18291] 40			44	1
Max. Cont.	95 [25]	1			354 [3129] 45	891 [7883] 45	1428[12636] 45	1971 [17445] 43			46	1
Max. Inter.	114 [30]					430 [3803] 54	959 [8485] 54	1492 [13207] 53			55	1
		-	0				_					-
	Rotor Width		Overall Effic			40 - 69%	0 - 39%					
	177.9 [7.003]		574 [5084]	1149 [10167]	1723 [15251]	2298 [20334]	2872 [25418]	3447 [30502]	4021 [35585]			
	mm [in]	-	Displacemen	t tested at 54	°C [129°F] w	ith an oil visc	osity of 46cSt	[213 SUS]				

WT (700 Series) Heavy Duty Hydraulic Motor



PORTING



.

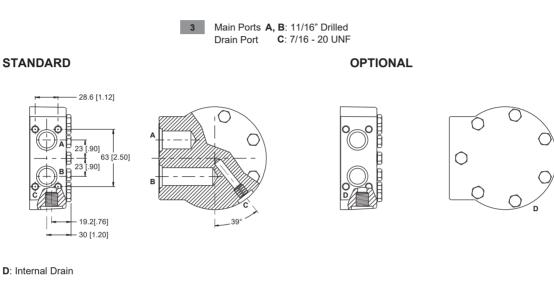
Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].



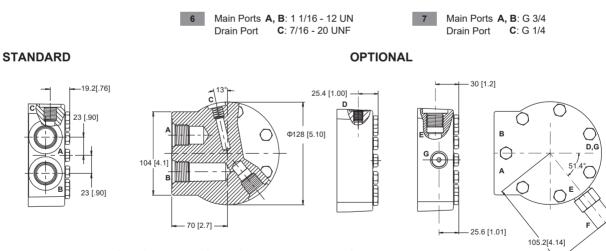


PORTING

SIDE PORTED - MANIFOLD ALIGNED



SIDE PORTED - ALIGNED



D: Internal Drain E: 10 Series/2-Way Valve Cavity 7/8-14 UNF G: Internal Drain Placement With Valve Cavity F: Valve Cartridge Installed

Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

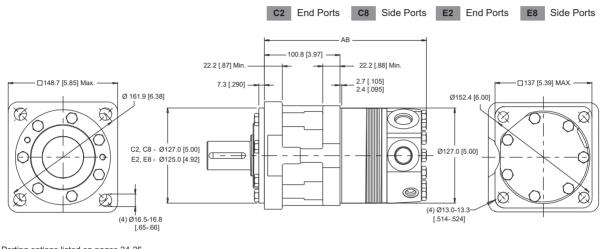
WT (700 Series)



Heavy Duty Hydraulic Motor

HOUSINGS

4-HOLE, SAE C MOUNT



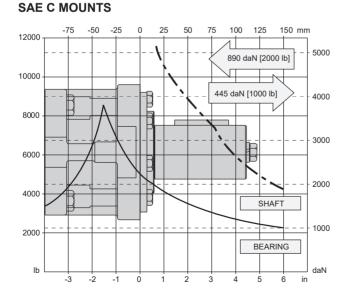
Porting options listed on pages 24-25.

Dimensions shown are without paint. Paint thickness can be up to 0.13 [.005].

TECHNICAL INFORMATION

ALLOWABLE SHAFT LOAD / BEARING CURVE

The bearing curve represents allowable bearing loads based on ISO 281 bearing capacity for an L_{10} life of 2,000 hours at 100 rpm. Radial loads for speeds other than 100 rpm may be calculated using the multiplication factor table on page 8.



LENGTH & WEIGHT CHART

Dimension AB is the overall motor length from the rear of the motor to the mounting surface.

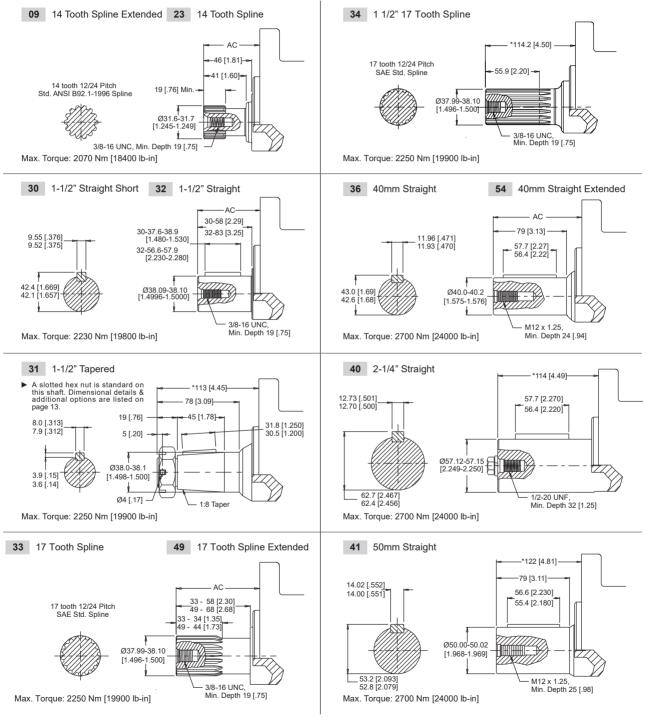
AB	Endcovers on pg. 24 mm [in]	Endcovers on pg. 25 mm [in]	Weight kg [lb]		
300	206 [8.14]	209 [8.25]	20.2 [44.6]		
375	213 [8.39]	216 [8.50]	20.8 [45.8]		
470	220 [8.69]	223 [8.80]	21.4 [47.1]		
540	227 [8.93]	230 [9.04]	21.9 [48.2]		
750	245 [9.64]	248 [9.75]	23.3 [51.3]		
930	260 [10.24]	263 [10.35]	24.4 [53.8]		
1K1	270 [10.64]	273 [10.75]	25.3 [55.7]		
1K5	308 [12.14]	311 [12.25]	28.3 [62.5]		
2K1	359 [14.14]	362 [14.25]	32.3 [71.3]		

 All WT series motor weights can vary ± 1.4kg [3 lb] depending on model configurations such as housing, shaft, endcover, options etc.





SHAFTS



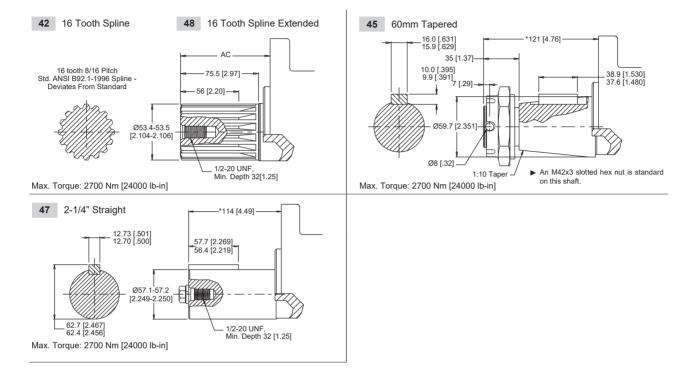
Dimension AC is charted on page 28.

WT (700 Series)



Heavy Duty Hydraulic Motor

SHAFTS



MOUNTING / SHAFT LENGTH CHART

Dimension AC is the overall distance from the motor mounting surface to the end of the shaft and is referenced on detailed shaft drawings on page 27.

AC	Length mm [in]	AC	Length mm [in]
09	86 [3.38]	36	113 [4.45]
23	64.7 [2.55]	42	91 [3.57]
30	77 [3.02]	48	121 [4.77]
32	113 [4.45]	49	99 [3.89]
33	68 [2.69]	54	121 [4.78]

Shaft lengths vary ± 0.8 mm [.030 in.]



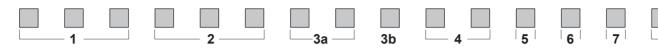
700 Standard Motor

WT (700 Series)

Heavy Duty Hydraulic Motor

ORDERING INFORMATION

1. CHOOSE SERIES DESIGNATION



5. SELECT A PAINT OPTION

- Black Α
- В Black, Unpainted Mounting Surface
- Ζ No Paint

6. SELECT A VALVE CAVITY / CARTRIDGE OPTION

F

Α None ▶ The 700 series is bi-directional. Reversing the inlet hose will reverse shaft rotation.

- В Valve Cavity Only 69 bar [1000 psi] Relief
- G 138 bar [2000 psi] Relief J 173 bar [2500 psi] Relief
 - 207 bar [3000 psi] Relief

121 bar [1750 psi] Relief

С 6 bar [1250 psi] Relief

2. SELECT A DISPLACEMENT OPTION	
300 300 cm³/rev [18.3 in³/rev] 930 929 cm³/rev [56.7 in³/rev] 375 374 cm³/rev [22.8 in³/rev] 1K1 1047 cm³/rev [63.9 in³/rev] 470 464 cm³/rev [28.3 in³/rev] 1K5 1495 cm³/rev [91.2 in³/rev] 540 536 cm³/rev [32.7 in³/rev] 2K1 2093 cm³/rev [127.7 in³/rev]	D 86 bar [1250 psi] Relief L 207 bar [3000 psi] Rel E 104 bar [1500 psi] Relief ▶ Valve cavity is not available on port option 3.
750 747 cm ³ /rev [45.6 in ³ /rev]	7. SELECT AN ADD-ON OPTION A Standard
3a. SELECT MOUNT TYPE 3b. SELECT PORT SIZE	B Lock Nut C Solid Hex Nut
▼END MOUNTS▼END PORT OPTIONSC2SAE C Mount (5" Pilot)17/8-14 UNF OffsetE2SAE C Mount (125mm Pilot)17/8-14 UNF Offset▼SIDE MOUNTS▼SIDE PORT OPTIONSC8SAE C Mount (5" Pilot)2G 3/4, RadialE8SAE C Mount (125mm Pilot)311/16" Hole, Aligned Manifold	 W Speed Sensor, Dual, 4-Pin Male Weatherpack Connector X Speed Sensor, Dual, 4-Pin M12 Male Connector Y Speed Sensor, Single, 3-Pin Male Weatherpack Connector Z Speed Sensor, Single, 4-Pin M12 Male Connector
5 1 1/16-12 UN, Radial 6 1 1/16-12 UN, Aligned 7 G 3/4, Aligned 4. SELECT A SHAFT OPTION	 8. SELECT A MISCELLANEOUS OPTION AA None AB Internal Drain AC Freeturning Rotor AD Internal Drain & Freeturning Rotor
09 14 Tooth Spline Extended 40 2-1/4" Straight	

LECT A MISCELLANEOUS OPTION

- lone
- nternal Drain
- reeturning Rotor
- nternal Drain & Freeturning Rotor

09	14 Tooth Spline Extended	40	2-1/4" Straight
23	14 Tooth Spline	41	50mm Straight
30	1-1/2" Straight Short	42	16 Tooth Spline
31	1-1/2" Tapered	45	60mm Tapered
32	1-1/2" Straight	47	2-1/4" Straight
33	17 Tooth Spline	48	16 Tooth Spline Extended
34	1 1/2" 17 Tooth Spline	49	17 Tooth Spline Extended
36	40mm Straight	54	40mm Straight Extended
_			

▶ For options not listed in the table above, please contact us with your requirements.